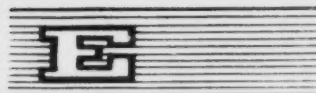




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RECENT TECHNOLOGICAL ADVANCES IN THE EXPLOITATION  
AND USE OF COAL RESOURCES

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## 1. Summary

Coal, in the near wide range of the world's fossil fuel resources, the magnitude of reserves identified is more definite. However, reflects the amount of exploitation has not been. Thus a judgement of the extent of coal is made. Thus less well known regions may have a significant resource. New oil and gas reserve techniques make it possible to estimate with an fairly the quantity of coal in a deposit.

Coal has a significant price advantage over oil or a thermal nuclear fuel. This is offset by better oil and infrastructure left and right. Particularly in consuming countries. Land transport of coal is seen as a potential limit to the introduction of land of new countries which are not traditional. Examples: New transport techniques such as rail pipelines may be important to the development of railway networks, although availability of water in some African countries could be a problem.

The range between coal and oil prices determines the extent to which coal can be treated as reserve oil more closely, or to which coal will be primarily used in developing countries. Coal is a reserve oil product.

Coal mining techniques sufficient for most types of coal deposits is well developed. Improvements in efficiency, however, still with mining of thick and steeply inclined coal seams are being developed as a number of countries.

Transit of coal, however, needs to be developed and new ways developed in order that oil-fired power and oil can be converted to coal with an economic advantage. Systems: New technologies for newly installed oil-fired units - especially in the power of the gas, ease of handling of the coal and its conversion with a greater degree of automation. The development and demonstration of coal-liquid mixtures offers a viable alternative to oil-fired and oil-fired coal mixtures.

Research and development activities which are taking place under the auspices of the International Energy Agency are designed to improve the understanding of coal technology and to enhance the adaptation for oil-fired coal use.

The image of coal as unattractive fuel which is difficult to handle, burn and which produces troublesome wastes at various stages in the chain of use is being put to rest. Its availability is unquestioned and its potential extensive.

## 2. The Nature of Coal

Coal is a highly variable, non-homogeneous fossilized material from ancient plants which has been converted as a result of exposure to high temperatures in the earth's crust over long periods of time, supplemented by the effects of pressure. It consists mostly of carbon compounds derived from dead organic matter but it also contains minerals and elements from the earth's crust. The degree of metamorphosis from living plants to peat, lignite, sub-bituminous coal, bituminous coal and finally anthracite represents the rank of the coal. As the rank increases so does the carbon content while the volatile matter contained in the coal decreases. The rank of a coal indicates its composition and how it will behave during processing, although the relationship of a coal property to its rank can only be defined in broad terms even within the same coal deposit.

Just about all of the elements in the earth's crust have either been identified in coal or are likely to be present. The major elemental components of coal are carbon, hydrogen and oxygen. Of the minor elements, silicon, sulphur, nitrogen, aluminium, iron, calcium and magnesium are predominant. The carbon combined with small amounts of hydrogen and oxygen, provides the structural integrity and most of the heat content of coal.

The total amount of mineral matter in coal varies considerably, but it is usually present in sufficient concentrations to be significant in any coal use. The most abundant minerals present in coal are the clay minerals (aluminosilicates), followed by sulphides, carbonates and silica.

The classification of different types of coal into operational categories for use internationally is difficult for two particular reasons:

- Divisions between coal categories vary between classification systems, both national and international, based on calorific value, volatile matter content, caking and coking properties, or some

continuation of these criteria. Although the relative value of coals within a particular category depends on the degree of dilution by moisture and ash and contamination by sulphur, chlorine, phosphorous and certain trace elements, these factors do not affect the divisions between categories.

- Coal quality can vary, and it is not always possible to ensure that the descriptive and analytical information which is available is truly representative of the body of coal to which it refers.

### 3. Coal Resources and Reserves

Total world coal resources are so large (Table 1) that if all were recoverable, they could provide thousands of years of supply. While these figures may be reassuring at first glance, they do not provide much information on possible constraints to the development and exploitation of coal as a source of energy.

Table 1

#### World Coal Resources and Reserves (Thousand million tonnes)

|                                | Bituminous Coal<br>and Anthracite | Sub-bituminous<br>Coal | Brown Coal/<br>Lignite |
|--------------------------------|-----------------------------------|------------------------|------------------------|
| Proved Reserves                | 774.6                             | 221.6                  | 323.5                  |
| Additional Resources           | 6164.4                            | 3835.2                 | 2159.6                 |
| Total Resources                | 6796.0                            | 4056.81                | 2483.1                 |
| Proved Recoverable<br>Reserves | 487.7                             | 143.0                  | 251.1                  |

Source: World Energy Conference, Survey of Energy Resources, 1980.

The IEA's World Coal Resources and Reserves Data Bank Service has undertaken a detailed study of coal deposits throughout the world, identifying those considered capable of playing a significant part in world coal supply and trade in the next 20 years. For practical purposes, a 20 year period is a reasonable planning horizon because:

- Any coalfield which will make a significant impact on the world market must already be well known and reasonably accessible to existing facilities. Undeveloped fields remote from ports, railways and centres of population are unlikely to play a significant role within 20 years.
- Any mining technology which will play a dominant part in 20 years time has already been invented and will take that long to spread through the industry.

For each of the significant coalfields an estimate has been made of the amount of coal which is accessible for working by current technology. Results of this work are summarized in Table 2 and published in the "Concise Guide to World Coalfields"\*.

Comparison of data in Tables 1 and 2 indicates that only about 55 per cent of the proved recoverable reserves identified by the World Energy Conference are considered by IEA Coal Research to be accessible over the next 20 years. This implies that although actual reserves are not a constraint to development, existing technology and economics do limit the availability of even proved recoverable reserves.

According to Table 2, reserves in OECD countries account for about one third of the world's total accessible coal with the United States alone having over 20 per cent. African countries account for about 6.5 per cent of the total, most of which is in South Africa.

It is necessary to keep in mind, however, that the large reserves in the United States and other OECD countries are partly due to the extensive exploration which has taken place. In future years, non-OECD countries may greatly increase their share of total world accessible coal as the infrastructure necessary to enable the mining and transport of coal is developed.

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\* Concise Guide to World Coalfields (IEA Coal Research, London, 1983)





the world's largest coal-producing group, accounting for almost 35 per cent of total world coal production, while the share of OECD coal production in world total coal output declined from 41 per cent in 1960 to 36 per cent in 1973.

From 1973 to 1981, total world coal output grew by 25 per cent. Coal production in the OECD during this period showed a considerable increase of almost 27 per cent, a significant acceleration from earlier trends. Thus, the share of OECD coal production in world total coal output has remained relatively constant around 36 per cent, since 1973.

Table 3  
World Total Coal Production by Regions  
(Million tonnes)

|             | 1960   | 1973   | 1978   | 1981   |
|-------------|--------|--------|--------|--------|
| World Total | 2600.5 | 3032.8 | 3494.8 | 3791.2 |
| OECD        | 1073.2 | 1104.4 | 1185.9 | 1398.4 |
| OPE         | 1420.2 | 1750.6 | 2068.7 | 2081.3 |
| All others  | 107.1  | 177.8  | 240.2  | 111.5  |

Source: IEA/OECD Coal Statistics and U.N. Energy Statistics

The overall coal production trends as indicated by Table 3 cover both hard coal and brown coal. A more detailed picture is given in Table 4 for Hard Coal. No brown coal production is reported as taking place in Africa.

OECD hard coal production fell by 2.7 per cent from 1960 to 1973. Production then increased by 3.2 per cent from 1973 to 1978 but accounted for less than 10 per cent of the total world production increase during this period. However, in the years since 1978, OECD production has increased by 17 per cent, representing about 7 per cent of the total world increase between 1978 and 1981. Substantial production increases after 1973 were recorded in Australia and the United States which more than compensated for the reduction of two major OECD European producers (Germany and the United Kingdom). The bulk of the increase in non-OECD production from 1973 to 1981 was assumed by China (163 Mt), the USSR (49 Mt), India (45 Mt) and the Republic of South Africa (68 Mt). Together they represent about 30 per cent of the total world hard coal production increase between 1973 and 1981 (367 Mt).

Table 4

Hard Coal Production by Regions/Countries  
(Million tonnes)

| Regions/Countries       | 1960   | 1973   | 1978   | 1980   | 1981   |
|-------------------------|--------|--------|--------|--------|--------|
| TOTAL WORLD             | 1966.9 | 2183.0 | 2545.7 | 2718.0 | 2750.2 |
| <u>OECD (1)</u>         | 935.8  | 910.5  | 940.9  | 1093.3 | 1097.9 |
| Canada                  | 6.4    | 12.3   | 17.1   | 20.2   | 21.7   |
| United States           | 391.5  | 529.6  | 576.8  | 710.4  | 698.1  |
| Australia               | 21.9   | 55.5   | 71.8   | 76.6   | 92.1   |
| Germany                 | 148.0  | 103.7  | 90.1   | 94.5   | 95.5   |
| United Kingdom          | 196.7  | 130.2  | 121.7  | 128.2  | 125.3  |
| Other OECD              | 171.3  | 79.1   | 63.3   | 63.6   | 65.1   |
| <u>NON-OECD (2)</u>     | 1031.1 | 1295.1 | 1604.8 | 1634.8 | 1642.3 |
| AFRICA                  | 39.7   | 68.4   | 95.9   | 121.7  | 136.9  |
| Botswana                | -      | -      | 0.3    | 0.4    | 0.4    |
| South Africa            | 38.2   | 62.4   | 90.6   | 116.0  | 131.2  |
| Zimbabwe                | -      | 3.5    | 3.1    | 3.1    | 2.9    |
| Other Africa            | 1.5    | 2.5    | 2.0    | 2.2    | 2.4    |
| ASIA                    | 486.6  | 557.1  | 756.9  | 767.6  | 782.2  |
| China                   | 420.0  | 430.0  | 593.0  | 574.0  | 593.0  |
| India                   | 52.6   | 77.9   | 101.5  | 109.1  | 123.1  |
| Other Asia              | 14.0   | 49.2   | 62.3   | 64.5   | 66.1   |
| USSR                    | 355.9  | 461.2  | 501.5  | 492.9  | 510.0  |
| EAST EUROPE             | 141.5  | 196.7  | 233.0  | 243.7  | 202.6  |
| Czechoslovakia          | 26.2   | 27.8   | 29.2   | 28.3   | 27.2   |
| Poland                  | 104.4  | 156.6  | 192.6  | 193.1  | 163.0  |
| Germany (GDR)           | 2.7    | 0.8    | 0.1    | -      | -      |
| Other East Europe(3)    | 8.1    | 11.5   | 11.1   | 12.2   | 12.4   |
| CENTRAL & SOUTH AMERICA | 7.3    | 11.6   | 17.5   | 19.0   | 20.6   |
| Colombia                | 2.6    | 3.0    | 4.8    | 5.3    | 5.3    |
| Mexico                  | 1.8    | 4.3    | 6.8    | 7.0    | 8.1    |
| Venezuela               | -      | 0.1    | 0.1    | -      | -      |
| Other C & S America     | 2.9    | 4.3    | 5.9    | 6.6    | 7.2    |

(1) Source: IEA/OECD Coal Statistics

(2) Source: United Nations Energy Statistics

(3) Includes Bulgaria, Hungary, Rumania and Yugoslavia

The distinction between coking coal and steam or thermal coal is important in projecting coal demand and for related production and trade forecasts, because the big producers of coking coal are limited in number and the big consumers are major steel-producing countries.

### Future Prospects

Given the amount of accessible coal in significant coalfields both within the OECD area as well as in non-OECD coal-producing areas, ultimate availability of coal is very large. Ample supply potential exists in existing and new mines in Australia, Canada, South Africa and the United States which could meet expanded coal demand. However, massive development of new coal production capacity and construction of the necessary infrastructure for coal transportation requires long lead times and without assured or firm expectations of substantial continuing growth in coal demand, the necessary investments may not be made. Therefore, actual coal production capacity will largely be determined by demand for coal.

Table 5

OECD Projected Coal Production  
(Million tonnes of coal equivalent)

|                    | 1978  | 1980  | 1985  | 1990   |
|--------------------|-------|-------|-------|--------|
| <u>Coking Coal</u> |       |       |       |        |
| <u>OECD TOTAL</u>  | 220.0 | 249.2 | 282.0 | 290.2  |
| CANADA             | 17.2  | 13.8  | 25.9  | 28.6   |
| UNITED STATES      | 80.2  | 104.7 | 120.1 | 120.1  |
| AUSTRALIA          | 40.2  | 46.8  | 52.9  | 57.2   |
| NEW ZEALAND        | 0.2   | 0.3   | 0.6   | 1.4    |
| JAPAN              | 9.1   | 8.5   | 6.3   | 6.6    |
| GERMANY            | 31.0  | 55.8  | 52.9  | 52.9   |
| UNITED KINGDOM     | 10.4  | 6.5   | 7.2   | 7.2    |
| OTHER EUROPE       | 15.6  | 14.8  | 15.1  | 16.2   |
| <u>Steam Coal</u>  |       |       |       |        |
| <u>OECD TOTAL</u>  | 642.2 | 757.1 | 843.5 | 1022.1 |
| CANADA             | 3.2   | 5.0   | 10.3  | 28.5   |
| UNITED STATES      | 447.3 | 533.7 | 596.3 | 735.0  |
| AUSTRALIA          | 26.4  | 38.1  | 64.1  | 76.8   |
| NEW ZEALAND        | 1.6   | 1.8   | 2.6   | 3.8    |
| JAPAN              | 10.3  | 12.0  | 12.9  | 13.3   |
| GERMANY            | 37.0  | 37.5  | 24.3  | 15.8   |
| UNITED KINGDOM     | 87.6  | 96.6  | 95.8  | 93.0   |
| OTHER EUROPE       | 29.4  | 37.1  | 27.3  | 36.0   |

Sources: IEA/OECD Coal statistics and IEA Country Submissions (1987)

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As can be seen from Table 5, the United States will continue to be the largest single coal producer during the next ten years, providing 60 per cent of total OECD coal output. The country has available coal reserves large enough to support rapidly expanding domestic and export needs. Uncertainty in domestic electricity generation growth is the major constraint facing coal production.

Australia's share would also increase from 7 per cent of OECD output in 1981 to 12 per cent by 1990, providing 25 per cent of incremental coal production. Ample potential for expanded production from existing and new mines exists with the commercial groups involved seeking long-term contracts. Currently, a number of new mine development plans are under way in New South Wales and Queensland. The major constraint on developing new mines is the current reluctance of consumers to enter into long-term commitments with adequate pricing arrangements which would provide the basis for the investment to develop new mines and associated infrastructure.

Canada is projected to increase coal production from 35 Mtpa in 1981 to 60 Mtpa in 1990. Coal resources are estimated to be adequate to supply an increasing domestic demand and an expanded export market. A major factor is that the main coal resources are located in the middle west of the country, separated from current domestic markets in the east by long distances and from western exporting terminals by difficult terrain, underscoring the importance of mastering future transport cost development.

Coal production in OECD Europe is projected to show a moderate increase from 313 Mtpa in 1981 to 330 Mtpa in 1990, as Spain, Greece and Turkey foresee a substantial expansion of output, mainly of lignite. Most other countries are estimated to maintain their current production level. Japan's production level is estimated to be around 19 Mtpa over the next ten years.

A number of non-OECD countries have the potential capability to supply future coal demand. The Republic of South Africa has large reserves available at competitive cost in the international market and is expected to increase its exports. Colombia is developing a coalfield near the Atlantic coast and has the potential to be a big supplier to OECD Europe in the 1990s. Botswana has geographically favourable coal seams and could enter the international market towards the end of the century, depending on solutions for the transportation.



About 70 per cent of the internationally traded coal in 1981 was imported by OECD countries, mostly OECD Europe and Asia. In OECD coal trade, OECD Europe mainly imports coal from the United States, South Africa and Poland. About 19 million tonnes are exported by Australia to South East Asia and by the United States to South America, South and North Africa.

In the export side, the United States is the largest coal exporter. It exported 53.7 million tonnes of coal in 1981, 40 per cent of which was steam coal. Outside of the OECD, the Republic of South Africa exported a record level of 29.4 million tonnes, 40 per cent more than one year ago, about 30 per cent above the 1979 level. On the import side, Japan imported sharply from 40.6 million tonnes in 1979 to 55.1 million tonnes in 1981, due to reduced production, the expansion of production at a 5 per cent rate and priority given to the domestic market.

#### Future Prospects

Trade in steam coal is a relatively new phenomenon in international trade. For many years only coking coal was traded internationally. Although coking coal trade is expected to increase in absolute terms over the next 10 years, the expansion of the world steel industry is expected to produce a net increase in overall share of coal trade, while the growing demand for coal for power generation purposes will increase. Future growth in coal trade will be increasingly dominated by the expansion in steam coal.

The Republic of South Africa has increased its coal production from 1.5 Mtpa before 1975 to a record level of 48 Mtpa in 1981. The expansion of the Richards Bay Harbour on the South African east coast will increase coal export capacity to about 45 Mtpa. Development of the new coal fields will increase export levels to 45 Mtpa by the mid-1980s. Further expansion of coal exports was decided upon in September 1981 and coal production is expected to reach 80 Mtpa in the 1990s.

Colombia is developing a coalfield near the Atlantic coast with production expected to start in 1984 and reach 10 Mtpa in the early 1990s. Further development is projected toward the end of the century.

As mentioned above, the entry of Botswana into the international coal market toward the end of this century depends on the solutions for the transportation issues. Such a solution in Botswana would need the construction of a 1,500 km railway and the upgrading of the port of Walvis Bay in Namibia.

The projected large potential increase in coal trade depends not only on potential growth in electricity and other industrial demand for coal but also on the ability of the importing countries to continue upgrading coal handling and inland transportation systems on time. Development of the necessary infrastructure at both ends is necessary for future expansion of coal trade.

#### 6. Coal Transportation

The coal transportation infrastructure of the world can be divided into three categories: inland transport, ports and ships. The effective capacity of any coal transport system may, for a variety of reasons, be significantly less than the nominal capacity. It appears that inland transport infrastructure may give the greatest cause for concern in the longer term. The development of slurry pipelines may provide the best solution in areas where rail or barge transport proves to be inadequate.

#### 7. Coal Prices

The distinct difference in price trends between coal and oil has been the main factor in explaining the relative use of these fuels in the industrial sector and particularly for electricity generation. In addition to the incentive provided by relative price movements, environmental considerations and ease of handling also promoted the shift away from coal, particularly given the less sophisticated technology available to control emissions from coal burning in the 1960s.

Following the considerable increase in oil prices after 1973, coal prices also tended to rise but at a slower rate. Coal's competitive advantage over oil increased dramatically after 1973 and was further accentuated by the more recent price increases in oil prices in 1979 and 1980. More recently, however, world coal prices have declined under depressed economic conditions and are unlikely to increase in the short term while the oil market remains calm.

On a thermal basis, the price of coal, including an allowance for freight is generally less than half the cost of fuel oil. Minemouth costs amount for about half of the total delivered cost of coal, although substantial differences exist, depending on specific trading patterns. Roughly half the non production-related costs are inland transportation costs to export terminals, with the remaining half being maritime transportation and handling charges both at loading and unloading ports.

Price will continue to be a determining factor of the pace at which coal use expands. Although current price relationships are such that coal enjoys a substantial competitive advantage, many potential purchasers are uncertain about how coal prices will evolve in the long run relative to oil prices, and are reluctant to undertake long term commitments to switch to coal. While it is impossible to predict future price developments for oil or coal with any certainty, a number of factors suggest that if coal markets continue to operate competitively, the delivered price of coal in constant dollars may not increase much, if at all, over the next 20 years.

## 8. Coal Mining

### Coal Mining Techniques

Surface mining involves the excavation of earth and rock covering the coal seam which is located at a relatively shallow depth. Following the removal of the coal, the land surface is regraded incorporating the previously removed overburden.

The level of coal recovery from surface mines is significantly higher than that from underground mines (85 per cent: 60 per cent). In addition, productivity is higher and the capital costs are typically about half those for underground mines. In many cases it is possible, by selective extraction, or even by special preparation of the surface of the coal seam, to significantly increase the quality of surface mined coal, whereas in a deep mined coal seam there is much less scope for flexibility in extraction.

Techniques for careful control of the mining operation to avoid pollution of the surrounding area together with reclamation of the mined site are well established. In many cases older mine sites are now being progressively restored.

There are two basic methods of underground mining; room and pillar and longwall. The room and pillar method involves the removal of coal to about 3 metres thick, whereas, longwall mining involves the removal of coal to about 1 metre thick. Longwall mining, basically because of the nature of the coal seam, is the most efficient method of underground mining.

The width of the coal face is determined by the size of the mining equipment used, the width of the coal seam and the strength of the pillars created. Large pillars are created to support the roof of the coal seam and ultimately sets a limit on the area of coal that can be mined. In some cases, restrictions on subsidence (the final limit of the coal seam) may, in some method, the removal of the pillars can be avoided.

Longwall mining allows better utilization of the coal seam, the development work per tonne of coal mined is lower, as is the cost of the coal, productivity rates, the proportion of coal lost to the waste rock is lower. The coal getting equipment, removes coal from the entire coal seam and the entire coal face. In the longwall method, the coal is mined in a long section behind the coal face. The coal is mined in a long section (often up to 150 metres) between the coal face and the waste rock.

Development is extensive for longwall mining and is a major factor in the better utilization of equipment. Longwall mining is a continuous process where jets, hydraulic ramming and removal, control, and other equipment are designed to increase coal production. Longwall mining is a continuous process also underway to optimize the extraction of coal from the coal seam and coal deposits.

### Recovery Ratio

In the United States, for example, the average recovery ratio for coal surface mines is about 80 per cent and for underground mines is about 60 per cent. Thick, single seam coal seams often have recovery ratios in excess of 95 per cent. The reason for this is that the coal seam boundaries in a small fraction of the total coal seam are not recovered after they are not recovered. The reason for this is that the coal seam boundaries, because this coal is a relatively thin layer, the recovery ratio is matter than the remainder of the seam. The recovery ratio for a coal seam will often have a lower recovery ratio than the recovery ratio for a coal seam of certain thickness of coal is just for coal that is recovered from the coal seam the surrounding material.

The recovery rate for underground mining is generally lower than for surface mining, since a certain amount of ore must be left in place around access for lifting. Additionally, more ore must be left in place around the perimeter of the property to be mined to provide support for the rock and prevent an excessive amount of ground movement.

Recovery rates for open-pit mining are generally higher, ranging from about 80 per cent depending on the width of the ore body to the width of the pillars. In the pillar case, the recovery rate is determined by the room and pillar sizes. About 50 per cent of the ore is typically recovered; the recovery rate, including the ore in the pillars, is about 80 per cent. The recovery rate is also affected by the size of the ore body, the depth, the larger the pillars must be, the lower the recovery rate.

Recovery rates for large-scale mining are generally higher than for small-scale mining, about 80 per cent. The recovery rate for large-scale mining is generally significantly higher than for small-scale mining, and the recovery rate for large-scale mining have been higher than for small-scale mining.

In date, the expansion of the mining industry is expected to be a significant potential advantage in terms of increased production and productivity, reduction in the overall cost per tonne of coal, the reduction in the number of underground workers, and a reduction in the number of underground workers. Nevertheless, the high cost of the mining industry in some cases a barrier to its expansion.

Haulage of coal and minerals from the surface to the surface is generally by means of conveyor systems. The conveyor systems have been tested include the use of air and water for conveying coal for crushed coal in pipelines. These innovations will have a significant impact on coal beneficiation activities.

Remote mining techniques are still in the early stages of development. The degree of control which can be achieved over the quality of the ore and the size distribution of the product is still a major area of research and development.

## 9. Coal Combustion

Irrespective of the variety of coal types, there are basic differences which affect the use of coal. Coal is a solid fuel and without quite extensive treatment it cannot be pumped like oil. Every movement of coal requires mechanical plant (scrappers, conveyors, etc.) which are considerably more complicated than the pumps and pipelines associated with oil products. Because of the solid nature of coal, which causes considerable wear of equipment, coal plants generally require more supervision and maintenance than comparable oil plants.

Combustion of coal is less intense than that of oil and gas. Thus for many applications a larger coal-fired boiler is required for a given heat output. The difference in combustion characteristics is also significant when considering the conversion of an oil, or more importantly, gas-fired installation to coal.

The ash content of coal is far higher than that of oil and the ash must either be removed by pre-combustion treatment or, more usually, be collected and disposed of after combustion. This feature has tended to mitigate against the use of coal in smaller installations, partly because of the extra equipment required and partly for lack of space. Newly developing coal cleaning technologies, however, as well as small-scale but extremely effective ash collecting systems, offer the prospect of far easier control of ash emissions.

The advantages of using coal stem from its price compared with the price of oil and also from its widespread availability. As noted above, on a thermal basis, the delivered price of coal is a little less than half that of fuel oil. This margin is extremely important as it governs the extent to which the coal price can absorb the cost of treating the impurities, waste materials and pollutants in order to satisfy the various regulations governing the use of coal, and the extent to which coal can be transformed into a form which is as convenient to use as the fuel it replaces.

### Conversion from Oil Firing to Coal

Generally the major problems for reconvertng a coal designed unit which has been burning oil are economic rather than technical. They include whether

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space is available for the reinstallation of coal handling and storage facilities, and whether equipment such as pulverizers, burners, electrostatic precipitators and ash handling facilities need to be reinstalled or replaced.

The direct firing of coal in a unit which was designed to burn oil involves a more extensive evaluation. Potential problems may include:

- . Furnace size inadequate for more than 50 to 70 per cent of rating
- . Excess air insufficient for complete coal combustion
- . Gas velocity too high in convection bank causing erosion
- . Tubes spaced too closely in convection bank permitting ash to bridge tubes
- . Lack of provision for ash and slag removal
- . Excessive temperature of gas entering convection bank causing slag formation and fouling
- . Use of finned tubes on economizer not compatible with coal ash
- . Preheater design incompatible with coal combustion
- . Inadequate electrostatic precipitator capacity
- . Inadequate control systems for coal combustion
- . Lack of burners for coal firing
- . Lack of coal handling system
- . Inadequate fan power.

This formidable list may not be applicable in all cases, but it is sufficient to make conversion to direct coal firing completely infeasible in many cases.

The development of coal liquid mixtures as one way in which coal may be introduced in a form with which the consumer may more readily identify. The coupling of coal gasification facilities to industrial systems is never likely to be an economic proposition. However, the possibilities of a centralized coal gasification facility providing fuel for a number of cities and industries should not be overlooked.

Some change in performance in terms of output is to be expected in converting from oil to coal. The extent of the change is a function of the specific design and current use patterns. The rated output of a boiler originally designed for oil is approximately proportional to the density of coal to be burned. Estimates of derating for oil-designed boilers after conversion to various forms of coal firing vary from 10 to 50 per cent.

#### Coal Combustion Technologies

Depending on the application and size of furnace, a number of combustion technologies are in widespread use. In industrial systems, various types of stoker-boilers are generally used. Stokers mechanically feed the coal on to a grate within a furnace and remove the ash after combustion. Table 1 characterizes various types of stokers.

Table 7  
Characteristics of Various Types of Grates

|                                     | Typical Capacity<br>Range<br>(kg steam/hr) | Maximum<br>Burning<br>Rate<br>(kg steam/hr<br>sq ft) | Characteristics                                                                                                                                      |
|-------------------------------------|--------------------------------------------|------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------|
| Spreader                            |                                            |                                                      |                                                                                                                                                      |
| Stationary and<br>dumping grate     | 10,000-15,000                              | 1.4                                                  | Capable of burning a wide<br>range of coals, best ability<br>to follow fluctuating loads,                                                            |
| Travelling grate                    | 45,000-180,000                             | 2.4                                                  | high fly ash carryover, low<br>load losses                                                                                                           |
| Vibrating grate                     | 10,000-45,000                              | 1.3                                                  |                                                                                                                                                      |
| Underfeed                           |                                            |                                                      |                                                                                                                                                      |
| Single or double<br>retort          | 10,000-15,000                              | 1.3                                                  | Capable of burning caking<br>coals and a wide range of<br>coals (including                                                                           |
| Multiple retort                     | 15,000-725,000                             | 1.9                                                  | anthracite), high<br>maintenance, low fly ash<br>carryover, multiple for<br>continuous-load operation                                                |
| Chain grate and<br>travelling grate | 10,000-45,000                              | 1.5                                                  | Characteristics similar to<br>vibrating-grate spreaders,<br>except these spreaders<br>have lower efficiency in<br>burning sticky, caking coals       |
| Vibrating grate                     | 15,000-70,000                              | 1.3                                                  | Low maintenance, low fly ash<br>carryover, capable of<br>burning wide variety of<br>weakly caking coals,<br>excellent operation over<br>entire range |

1 kg. steam/hr = 1.0% MCR%

Source: Coal Handbook, R.A. Meyers, ed.

For larger installations, particularly power stations, pulverized coal  
(-200 mesh) is burned. There are several methods of firing pulverized coal  
which are related to the location and position of the burners in the furnace.  
The type of firing method used depends mainly on the type and size of the  
boiler and the coal type. Pulverized coal-fired boilers can fire a wide range

of coals. Although bituminous coals are by far the most common fuels, everything from anthracite to lignite has been fired in utility-size pulverized coal units. The effect of the ash in the coal on the operation of the furnace is an important aspect of coal selection. Most pulverized fuel furnaces are of the 'dry-bottom' variety in which the ash is removed as a dry solid. It is therefore necessary that the ash fusion temperature of the coal must be sufficiently high to avoid the ash slagging (becoming liquid). With pulverized fuel firing about 80 per cent of the ash is contained in the flue gases leaving the rest as 'bottom-ash'. It is this fly ash, which under certain circumstances, sticks to the furnace walls and/or the water tubes. Blowers are often used on a regular basis to dislodge ash deposits and prevent excessive buildup. The presence of iron and alkalis in the ash increases its adhesion to the furnace walls and water tubes.

Coal characteristics affect fuel preparation for pulverized fuel firing (moisture/handling; mineral matter/grinding), furnace operation and reliability (rating, availability/maintenance). Declining coal quality in recent years has resulted in a greater quantity of fuel being required to produce the same heat input. This puts extra loads on the pulverizers and the electrostatic precipitators. In the United States, for example, between 1969 and 1977, the mean heat rate for large coal-fired plants rose from 9,500 KJ/kWh to 10,000 KJ/kWh. Alternatively, boilers have been unable to maintain their rated capacity.

The cyclone furnace has, in many applications, been the main alternative to a pulverized fuel furnace, and although it is now no longer being installed there are a large number still in use. The furnace walls are water-cooled and covered with refractory brickwork. The high gas temperatures melt the ash which forms as a liquid slag on the furnace walls. Most of the ash is retained in the slag layer so that fly ash production is minimised, reducing fouling problems and electrostatic precipitator requirements. The main disadvantage of the cyclone furnace is the high level of NO<sub>x</sub> formation which results from the high gas temperatures.

Recent developments in pulverized coal firing include the direct firing of pulverized coal on a small scale. If the coal is of high enough quality (low ash, low moisture content) it is possible to burn it without the support of an auxiliary fuel such as oil or gas.

Demonstrations are underway in a number of countries of the direct firing of pulverized coal in small boilers (10-20 MW) using coal prepared in a central facility and delivered by tanker to a sealed storage bin adjacent to the boiler. Substantial savings have been made in operation costs, in one case enabling the cost of converting a 10 MW unit operating for 5,000 hours a year to be recouped in two years. Providing adequate precautions are taken, pulverized coal can be transported, handled and stored in a safe manner. Demonstrations on boilers of about 10 MW are being evaluated in Europe.

The main advantages of this system over coal water mixtures is that there is no inert material accompanying the coal.

### Fluidized Bed Combustion

Fluidized bed combustion of coal (FBC) is being developed as an alternative to stoker fired combustion for industry and pulverized coal combustion for electricity generation. Fairly small fluidized bed boilers and furnace type dryers (less than 20 MW), which operate at atmospheric pressure, have been commercially available in a number of countries for some time. The application of FBC to the generation of electricity is still under development.

A fluidized bed consists of a stream of gas flowing upwards through a dense bed of solid particles. As the gas flow rate increases so does the force exerted on the particles until the bed of particles appears to boil (bubbling bed). If the gas flow rate is increased further, the smaller particles become entrained in the gas stream and are removed. Increasing the gas flow even further causes all the particles to be transported from the bed. This latter stage is the principle of the circulating fluidized bed. The particles are subsequently separated from the gas in a cyclone and returned to the bed. Both bubbling and circulating fluidized bed combustion are under active development and are available in smaller sizes for the combustion of a variety of fuels including coal, washery wastes, wood chips and biomass.

Coal mixed with limestone is supplied continuously to the bed, and the ash remaining after combustion is removed to keep the volume constant. Because of rapid mixing and the high rate of coal combustion, the



The combustion temperature is half-way between the boiling temperature of the ash - that is, remains fairly throughout the process. The design of a fluidized bed boiler is therefore less dependent on fuel characteristics, or that of a conventional boiler.

Since the fluidized bed boiler is an efficient means of generating atmospheric pressure steam, it is well suited for use in a boiler without modification of design. A number of low capacity fluid bed boiler installations have been made, one of the first fluid bed boilers of the purpose-built type was available from a number of manufacturers in a size of 150 Mw. In general, capacities above the 100 Mw to 200 Mw range, while the largest AFBC units in commercial operation have a capacity of about 150 Mw, largest fluid bed boiler construction is planned.

In the operation of fluidized bed boilers, the boiler is a conventional boiler, although the fuel is fluidized. The design and construction of the system are the same as for a conventional boiler, and the boiler is used. The design of the boiler is the same as for a conventional boiler, and the boiler is used. The design of the boiler is the same as for a conventional boiler, and the boiler is used.

Fluidized bed boiler technology has been developed in a number of conventional fluidized bed boilers, and the design of the boiler is the same as for a conventional boiler. The design of the boiler is the same as for a conventional boiler, and the boiler is used. The design of the boiler is the same as for a conventional boiler, and the boiler is used. The design of the boiler is the same as for a conventional boiler, and the boiler is used.

Table 7

Comparison of Bubbling and Circulating AFBCs  
for Utility Applications

| <u>Characteristic</u>                    | <u>Type of FBC</u> |                    |
|------------------------------------------|--------------------|--------------------|
|                                          | <u>Bubbling</u>    | <u>Circulating</u> |
| Largest Existing Unit Mw(e)              | 20                 | 30                 |
| Combustion Efficiency                    | 99.0               | 99.9               |
| Ca:S for 90%SO <sub>2</sub> removal      | 2.3                | 1.5                |
| NO <sub>x</sub> , lb/10 <sup>6</sup> Btu | 0.4                | 0.4                |
| Feed points per 100 MW                   |                    |                    |
| Coal                                     | 6 stokers          | 2 pneumatic        |
| Limestone                                | 2                  | 2                  |
| Auxiliary Power, % of gross              | 5                  | 6                  |
| Steam generator Cost Ratio               | 1.0                | 1.05 to 1.15       |

Source: Electric Power Research Institute

The ability to use coal (and other fuels) with a high proportion of inert material makes fluidized bed combustion an attractive option for burning residues from coal preparation such as flotation tailings. Trials have been underway in Australia, Germany and the U.K. for some years resulting in the successful combustion of washery wastes by fluidized bed combustion.

The possibility of fluidized bed plants operating in conjunction with coal preparation plants, producing clean low sulphur coal at minimum cost, or coal-water mixtures, together with electricity or steam from the refuse high sulphur material, is one which is being considered by a number of countries, both on economic and on environmental grounds.

The advantages of fluidized bed combustion which are evident for large boiler plants, such as not requiring the installation of flue gas desulphurization and also the smaller size of boiler for a given output, are not, however, generally applicable to small industrial applications. These units operate on low sulphur fuels and so far, in most cases, do not require flue gas desulphurization anyway. Although at the moment low sulphur coal does not command much of a premium price, this may change thus favouring fluidized bed combustion.

Fluidized bed combustion is commercially available in a number of countries on the same basis as other boilers. The maximum size so far installed is about 130 MW and many of the installations have been designed to use what would otherwise be waste materials such as washery wastes or wood chips.

Although fluidized bed combustion with limestone addition can remove sulphur, this in itself creates a significant amount of solid waste material for subsequent disposal (this material may be used in the building industry if the sulphur content is not too high). When burning a high sulphur (4 per cent) coal for example and removing 90 per cent of the  $\text{SO}_2$  formed during combustion, up to 400 tons per hour of spent limestone would be produced from a 1000 MW power plant. Hence there is a significant incentive to develop systems that reduce the production of limestone sorbent and spent solids.

Recent investigations by EPRI suggest that atmospheric fluidized bed combustion which includes recycling of the bed material reduces limestone consumption, improves boiler and combustion efficiency and reduces capital and bus bar costs to the point that atmospheric fluidized bed/recycle systems are considered to be competitive with pulverized coal-fired systems with flue gas desulphurization using both high and low sulphur coal.

As well as varying the extent of fluidization, combustion can either take place at atmospheric pressure (AFBC) or under a pressure of 5 to 20 bar (PFBC).

Pressurised fluidized bed combustors of the bubbling-bed type are being primarily developed for the generation of electricity. The combustor operates at a high pressure, supplied via a gas turbine-driven air compressor. While the major part of the energy in the hot, pressurised exhaust gas is expended driving the air compressor, any excess energy can be used to generate electricity in a gas turbine to supplement that generated in a steam turbine in the normal way. A PFBC therefore can be operated in a combined cycle mode at an overall efficiency of about 40 per cent compared to about 35 per cent efficiency for a pulverized coal power plant equipped with a wet scrubber for removing  $\text{SO}_2$ .

In addition to the advantages normally associated with fluidized bed combustion, PFBC offers even further reduced boiler sizes which should permit

factory assembly even for quite large units, and a relatively simple concept relative to other combined cycles.

However in developing PFBC for commercial use, a number of issues must be satisfactorily resolved. These include:

- Efficient clean up of the hot gases prior to passing them over a turbine.
- Development of turbine blade materials for this application.
- Avoidance of erosion and corrosion of boiler tubes.
- Integration of combustor and gas turbine.
- Scale-up to utility plant size.

An alternative to the gas turbine combined cycle is the development of the turbocharged boiler which is based on PFBC but which has a much reduced gas turbine inlet temperature when compared to the combined cycle. The lower temperatures result in less stringent metallurgical demands and consequent improved reliability of the gas turbine and simplified structural design.

The turbocharged boiler, however, is not as efficient as a combined cycle plant, since there is no excess energy in the combustion gases to generate electricity. The advantage may well lie in this technology being a first step towards PFBC combined cycle, enabling the hot gas clean-up and turbine materials problems to be resolved separately.

Pressurised fluidized bed combustion technology for electricity generation is being pursued in two basic concepts; air cooled and steam cooled combustors for combined cycle generation of electricity. Variations on these two concepts such as using the gas turbine exhaust to support combustion in an AFBC to raise steam have also been studied, but so far little data has been accumulated.

Comparisons based on US Eastern and Western coals suggest that the cost of electric power from PFBC could cost up to 10 per cent less than that for a pulverized coal/flue gas desulphurization reference system. The costs for the

UK of fluidized bed combustion compared with pulverized coal firing for electricity generation have also been compared showing savings of a similar magnitude. There appear to be significant economies of scale for PFBC and conversely there are cost penalties associated with multimodular design. An air cooled PFBC system requires a much greater heat transfer surface than the steam cooled system and therefore on an equivalent thermal basis would be more expensive.

PFBC plant designs appear to be competitive with pulverized coal plant, but it should be noted that evaluations are so far based on preliminary design and operating data. There is no certainty that PFBC can meet stringent particulate emissions. The reliability of both hot gas clean up systems and pressurised fluidized bed combustors is being examined particularly in an IEA 80 MW (thermal) experimental facility built in the UK jointly by Gernay, UK and US. The extent to which these and other tests are sufficient for subsequent commercial development remains to be seen. Also, the tolerance of gas turbines to particulate material in the hot gases has yet to be defined and demonstrated. Other advantages of PFBC over AFBC accrue on the environmental side. Less limestone is required for  $SO_2$  removal and less  $NO_x$  is produced during pressurised fluidized bed combustion. On a very large scale (over 200 MW) PFBC is likely to be preferable to AFBC because of the greater (10 to 15 times) intensity of combustion.

Based on current developmental trends, however, it is unlikely that large scale PFBC (over 200 MW) will be available for utility use before 2000.

#### Coal Gasification - Combined Cycle

The major alternative development to the pulverized coal-fired boiler for electricity generation is to substitute coal gasification plant for the pulverized coal boiler. The production of medium calorific value gas (carbon monoxide and hydrogen) is possible by a number of different methods, some of which have been commercially available for many years, while others are still in the development stage. The gains in efficiency resulting from combined cycle generation of electricity are generally considered to be sufficient to offset the inherent losses associated with gasification of the coal. An additional advantage of combined cycle generation of electricity, relative to a conventional steam turbine of the same capacity, is the decrease of about 35 per cent in water requirements per unit of electrical output.

For use in a gas turbine, the raw gas from any coal gasification process must be cleaned of both particulate material and all other gases to prevent fouling and erosion of the turbine blades, to minimise the pollution of the atmosphere and to prevent solid particles interfering with the operation of the turbine.

The nature and concentration of the contaminants removed in the gasification process being used. In any case, gas cleaning efficiency in excess of 99.5 per cent will be required. If efficiency is to be maintained, both gas clean-up and sulphur removal must take place while the gas is hot (with FBC, sulphur removal takes place during combustion). It has been estimated that hot gas treatment could increase overall plant efficiency by about 2 per cent. The alternative is to cool the gases to about 400°C, transferring the heat in then to water which is turned to steam as part of the feed to the steam turbine.

Table 10 shows the development of hot gas particulate removal processes.

Table 10  
Hot Gas Particulate Removal Development  
Operating Conditions

|                            | Temp. °C | Pressure<br>Atm | Removal Efficiency                                           |
|----------------------------|----------|-----------------|--------------------------------------------------------------|
| Cyclone systems            | 650      | 5               | 99.5% (>40 micron),<br>1% (0 to 2.5 micron)                  |
| Multi-cyclone systems      | 650      | 50              | 99.5% (>0.5 micron),<br>50% (>2 micron)                      |
| Metal filters              | 800      | 50              | 99% (>10 micron), 5% (>20 micron)                            |
| Fibre filters              | 650-1200 | 1               | 100% (>1 micron)                                             |
| Fabric filters             | 1370     | 1               | 99.5% (at ambient temp.)                                     |
| Ceramic filters            | 760      | 1               | 100% (>1 micron)                                             |
| Bed filters                | 870      | —               | 99.5% of + 5 micron but may<br>generate sub-micron particles |
| Electrostatic precipitator | 800-1200 | 20              | 99% (> 5 micron),<br>98.5% (0.75 to 1 micron)                |

Some of the nitrogen in the coal is converted to ammonia and can be readily removed from the synthetic gas by a straight forward scrubbing process. The air used for combustion is the other source of nitrogen. The formation of nitrogen oxide in the turbine combustor is suppressed by adding moisture to the clean syngas to hold down the flame temperature. The final solid wastes from gasification combined cycle plants are quenched with water from the ash in the coal and sulphur, di-sulphide of which is straight forward.

The costs of combined cycle power plant compared with other processes are necessarily uncertain because of the stage of development of the processes and the consequent lack of information about system and component reliability. The 100 MW demonstration plant now under construction in the United States based on the Texaco gasification process is a waste heat recovery cycle is designed to fulfill the objectives by constructing an integrated coal gasification combined cycle electric generating facility on a scale capable of demonstrating:

- Compliance with environmental regulations
- Operational flexibility and reliability
- Coal feedstock flexibility
- Integrated systems controls
- Alternative plant and process components.

The facility will assist in the establishment of operating, maintenance, safety and training procedures and in the development of precise economic criteria.

#### Coal-Liquid Mixtures

Despite coal's extensive price advantage over oil and gas, the relative inconvenience and increased capital costs associated with coal use have largely limited coal to electric utility and larger industrial applications. The benefits of economies of scale in large facilities together with cheap fuel costs have tended to offset the high capital cost of ancillary equipment.

Overcoming the barriers to coal use will be greatly facilitated if the coal-based fuel is presented in a form similar to the fuel it is replacing. Coal-firing systems (CFM) have the potential to lower the cost of using coal by eliminating dust and slag and furnaces by providing the users with the convenience of a liquid which can be stored and distributed like oil and which can be pumped to specifications in a large centrally located facility.

Coal-oil slurries (COS) have been being tested in a variety of applications and a number of companies are preparing to supply COS on a commercial basis. However the current state of the oil market has reduced the economic attractiveness of COS in many countries with the notable exception of Japan. Coal water mixtures (CWM) are being developed and tested in a number of countries for a number of different applications in both boilers and furnaces. As well as having combustion characteristics, development of refinement techniques minimising the quantity of stabilising additives required is underway.

Progress in recent years in fine coal cleaning has provided a technological basis for the preparation of low ash, low sulphur fine coal for use in COS preparation. One of the attractions of CWM is that part of the water used in the cleaning process becomes the liquid phase of the slurry. The fine mill effluent stream in a coal cleaning system is a potential precursor to COS preparation. The preparation of low ash coal slurries could mean that a large number of furnaces designed for oil firing could be successfully converted to burn CWM with little or no de-rating, although the cost of the fine grinding required to ensure most of the ash to be removed in order to avoid wetting during, depending on the coal type, prove to be expensive.

The cost of converting boilers from oil to coal firing together with the attendant technical problems are the major drawbacks to fuel switching. Only a minority of the utility boilers originally designed to burn oil were built with coal-firing potential. Even the conversion of these boilers is likely to require considerable expenditure on coal handling equipment and on environmental control.

One of the major drawbacks of CWM is the extent to which the capacity of the boiler is reduced as a result of using a lower calorific value fuel and in the case of CWM the water which must first be evaporated. Conversion to CWM

firing would therefore generally entail keeping the original oil burning capability which may be required during start-up or at periods of low load (to maintain flame stability) or at maximum load to obtain the rated output of the boilers.

The ultimate development of COM may result in a fuel which is clean enough to be used in direct firing applications such as the brick and ceramic industries. In addition, low ash fluid coal made with ultrafine coal (less than 10 microns) may one day be suitable for use in gas turbines or even internal combustion engines. The particle size and size distribution is an important factor in preparing coal liquid slurries, particularly CWM where particle sizes down to 15 microns are being used.

Preparation of COM can be achieved in two basic ways; using pulverized coal with an additive to achieve a stable suspension and by using ultrafine ground coal, the preparation of which is expensive and depends to a large extent on coal type. COM needs to be warm when pumped and hot when atomized for combustion. Extensive tests with various coal:oil ratios have been carried out and generally little or no derating of conventionally shaped boilers occurs at coal concentrations of up to 50 per cent. There is, however, some derating of boilers with a relatively smaller volume than conventional configurations.  $\text{NO}_x$  emissions increase with increasing coal content and with the amount of excess air used. Emission of  $\text{SO}_x$  is dependent on the sulphur content of the fuel. Ash which is deposited during combustion is generally successfully removed by soot blowers which it is necessary to fit to the boiler. Erosion of the burners by the solid coal in the mixture has been lessened by providing hard facings to vulnerable areas.

Depending on the price and availability of oil, however, COM may turn out to be an interim fuel for industrial and utility use. Table 11 sets out the status of COM activities in the United States in 1982.

The more attractive proposition in the longer term is CWM in which all of the energy is provided by coal (even with a 50% by weight of coal in COM, only 40% of the energy is provided by coal). Following intensive cleaning of fine coal to less than 3 per cent ash and 1 per cent sulphur, the water content is adjusted to the 25 to 30 per cent range and the mixture is supplemented with additives to control the stability of the slurry and to reduce the viscosity. For extended periods of storage it is necessary to

1. The first part of the report deals with the general situation of the country and the progress of the work during the year.

2. The second part of the report deals with the results of the work done during the year and the progress of the various projects.

3. The third part of the report deals with the financial situation of the organization and the results of the financial work.

4. The fourth part of the report deals with the administrative work and the progress of the various administrative projects.

5. The fifth part of the report deals with the results of the work done during the year and the progress of the various projects.

6. The sixth part of the report deals with the financial situation of the organization and the results of the financial work.

7. The seventh part of the report deals with the administrative work and the progress of the various administrative projects.

8. The eighth part of the report deals with the results of the work done during the year and the progress of the various projects.

9. The ninth part of the report deals with the financial situation of the organization and the results of the financial work.

Table 1.

Table 1. (continued)

| Institution         | 1980-1981 |           | 1982-1983 |           | 1984-1985 |           | 1986-1987 |           | 1988-1989 |           |
|---------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
|                     | 1980-1981 | 1982-1983 | 1984-1985 | 1986-1987 | 1988-1989 | 1990-1991 | 1992-1993 | 1994-1995 | 1996-1997 | 1998-1999 |
| Adelphi University  |           |           |           |           |           |           |           |           |           |           |
| Allied Oil Company  |           |           |           |           |           |           |           |           |           |           |
| American Refining   |           |           |           |           |           |           |           |           |           |           |
| Group Company       |           |           |           |           |           |           |           |           |           |           |
| ARCO                |           |           |           |           |           |           |           |           |           |           |
| Brookhaven National |           |           |           |           |           |           |           |           |           |           |
| Lab.                |           |           |           |           |           |           |           |           |           |           |
| Castrol, Inc.       |           |           |           |           |           |           |           |           |           |           |
| CJBRG Research      |           |           |           |           |           |           |           |           |           |           |
| Products, Inc.      |           |           |           |           |           |           |           |           |           |           |
| Coastal Corporation |           |           |           |           |           |           |           |           |           |           |
| CONCO               |           |           |           |           |           |           |           |           |           |           |
| Columbia Pipeline   |           |           |           |           |           |           |           |           |           |           |
| Coal Energy Corp.   |           |           |           |           |           |           |           |           |           |           |
| BRASCO              |           |           |           |           |           |           |           |           |           |           |
| ERGON               |           |           |           |           |           |           |           |           |           |           |
| Florida Power       |           |           |           |           |           |           |           |           |           |           |
| (FPC)               |           |           |           |           |           |           |           |           |           |           |
| Florida Power &     |           |           |           |           |           |           |           |           |           |           |
| Light Co., Inc.     |           |           |           |           |           |           |           |           |           |           |
| Gulf-Western        |           |           |           |           |           |           |           |           |           |           |
| Industries, Inc.    |           |           |           |           |           |           |           |           |           |           |
| Intermountain Coal  |           |           |           |           |           |           |           |           |           |           |
| Island Creek Coal   |           |           |           |           |           |           |           |           |           |           |
| Co.                 |           |           |           |           |           |           |           |           |           |           |
| MTI                 |           |           |           |           |           |           |           |           |           |           |
| Mt. Airy Refining   |           |           |           |           |           |           |           |           |           |           |
| NEPSco              |           |           |           |           |           |           |           |           |           |           |
| Northeast Petro     |           |           |           |           |           |           |           |           |           |           |
| Ohio Univ. at Akron |           |           |           |           |           |           |           |           |           |           |
| PSTD                |           |           |           |           |           |           |           |           |           |           |
| Tufts               |           |           |           |           |           |           |           |           |           |           |
| University of Ma.   |           |           |           |           |           |           |           |           |           |           |
| UOP Incorporated    |           |           |           |           |           |           |           |           |           |           |
| Wyatt Oil           |           |           |           |           |           |           |           |           |           |           |

\* - Completed FID

Source: US DOE

4482E

Table 12 lists CDM preparation plants in the United States.

Table 12

United States CDM Preparation Plants  
(1982)

| Name of Company                                  | Location     | Capacity                  | Process Description                                                                         |
|--------------------------------------------------|--------------|---------------------------|---------------------------------------------------------------------------------------------|
| CC&Co.                                           | Florida      | $2.5 \times 10^3$ bbl/day | Ultrafine coal;<br>mechanical grinding                                                      |
| Island Creek<br>Coal Co.                         | Florida      | $5.0 \times 10^3$ bbl/day | Standard grind (80%<br>minus 200 mesh),<br>plant is relocatable                             |
| Allied Oil Company                               | Ohio         | $1.5 \times 10^3$ bbl/day | Standard grind (80%<br>minus 200 mesh), both<br>dry and wet grinding<br>techniques are used |
| Reafluid, Inc.                                   | Kentucky     | $1.2 \times 10^3$ bbl/day | 80% minus 200 mesh,<br>Cottrell Ultrasonic<br>Process                                       |
| Columbia Fluidized<br>Coal Energy<br>Corporation | Pennsylvania | $0.4 \times 10^3$ bbl/day | Standard grind (80%<br>minus 200 mesh)                                                      |

Source: US DOE

Table 13

Status of CWM Activities in the United States  
(1982)

| Company/<br>Institution                          | Activities | CWM PREPARATION |                |                     | CWM COMBUSTION |            |         |
|--------------------------------------------------|------------|-----------------|----------------|---------------------|----------------|------------|---------|
|                                                  |            | R/D             | Pilot<br>Plant | Commercial<br>Plant | R/D            | Evaluation | Furnace |
| Alfred University                                |            | X               |                |                     |                |            |         |
| ARCO                                             |            | X               |                |                     |                |            |         |
| Atlantic Research                                |            | X               | X              | Planned             | X              | X          |         |
| COMCO                                            |            | X               |                |                     |                |            |         |
| ERGON                                            |            | X               | x(1)           |                     | X              | x(1)       | x(1)    |
| Gulf-Western                                     |            | X               | X              |                     |                |            |         |
| Island Creek Coal/<br>Occidental Research<br>Co. |            | X               |                |                     |                |            |         |
| MIT                                              |            |                 |                |                     | X              |            |         |
| PETC                                             |            | X               | X              |                     | X              | X          |         |
| Slurrytech, Inc./<br>BAW                         |            | X               | X              | Planned             | X              | X          |         |

(1) ERGON developed and patented a coal pulverization process in which a fluid energy mill was used. The steam, a grinding medium, was also transported to the furnace. ERGON named it the coal/steam process.

Source: US DOE

A recently completed study in a number of IEA countries assessed the potential for CLM utilization based on oil-fired utility and industrial boiler populations in each of the countries. The boiler populations were categorized by design, type, age and size. Average capacity factors were used in conjunction with other parameters to estimate fuel oil consumption and the quantity of oil which could potentially be replaced by changing to CLM or CWM.

In the six participating countries (Canada, Japan, Netherlands, Sweden, US) the following utility and industrial boiler population was ascertained (Table 14).

Table 14

Boiler Population

| (a) <u>Utility</u>                           |                          |                                |
|----------------------------------------------|--------------------------|--------------------------------|
| <u>Design</u>                                | <u>Number of Boilers</u> | <u>Output MW (b)</u>           |
| Coal                                         | 135                      | 36928                          |
| Future Coal, Oil                             | 85                       | 10677                          |
| Mineral Oil                                  | 190                      | 85452                          |
| Compact Oil                                  | 267                      | 31672                          |
| Total                                        | <u>857</u>               | <u>176929</u>                  |
| total (less than 20 years old)               | <u>484</u>               | <u>141693</u>                  |
| (b) <u>Industrial</u>                        |                          |                                |
| <u>Design</u>                                | <u>Number</u>            | <u>Input Capacity (MW)(th)</u> |
| Coal                                         | 148                      | 14539                          |
| Modular/Field Oil                            | 6727                     | 229897                         |
| Package Water tube oil                       | 19819                    | 133750                         |
| Package Fire tube oil                        | 140821                   | 189522                         |
| Total                                        | <u>167515</u>            | <u>567704</u>                  |
| total (less than 20 years old,<br>over 3 MW) | <u>19032</u>             | <u>274605</u>                  |

Source: IEA CLM Project

In determining the magnitude of the potential market for CLM, boilers of less than 20 years old were considered possibilities for conversion and, in addition, in the industrial sector a lower limit of 3 MW(th) input was set.

The amount of oil which could be replaced by the utility sector switching to CLM is between 70 per cent and 85 per cent of the oil consumed depending on the amount of derating which is equivalent to about 700 million barrels a year in the six countries surveyed. The potential replacement of oil by CLM or CWM in the industrial sector is about 480 million barrels per year in the case of CWM and about 210 million barrels per year in the case of CLM representing about 50 per cent and 21 per cent respectively of the total oil consumed. The potential for African countries is unknown but it could well be that an equivalent proportion of the oil consumed in industrial and utility boilers could be replaced by coal-liquid mixtures.

In examining the economics of coal-liquid mixtures the gap between coal and oil prices (currently around \$3 per GJ) must be sufficient to cover the costs of cleaning the coal, slurry preparation, transport and storage, boiler conversion and any derating of the boiler.

### Pyrolysis

Pyrolysis, or the partial combustion of coal is one means of obtaining gaseous and liquid products from coal, leaving a residue of char which has some value as a fuel depending on the severity of the pyrolysis process. Pyrolysis can take place in an inert atmosphere or in an atmosphere which increases the amount and quality of the gaseous and liquid yields, such as hydrogen.

Depending on the ratio of organic to inorganic sulphur in the coal, and on the nature of the mineral constituents of the coal, the sulphur released during pyrolysis reacts with minerals in the coal to form sulphides. Thus after pyrolysis of a high sulphur coal, the sulphur content of the char may be high, but not much of it is released during combustion of the char (the sulphides are converted to sulphates which do not decompose until extremely high temperatures are reached). The sulphur which is released with the gases is readily recovered with commercially available processes in the same way as with coal gasification (see above). The extent and mechanism of the elimination of sulphur is under examination by a number of researchers who are obtaining desulphurization during pyrolysis but to different extents and by different methods depending on the nature of the coal and reaction conditions, but particularly on the way the organic sulphur is bonded to the coal molecule.

However the pyrolysis process itself would seem to require further improvement, regardless of the extent to which it can be a means of utilising high sulphur coals in a clean manner.

### 10. IEA Coal Research and Development

There are a number of collaborative R&D programmes aimed at the assessment and development of improved combustion techniques which are taking place under the umbrella of the IEA. These include the construction and operation of an 80 MW (thermal) pressurized fluidized bed combustion facility;

On the 10th of January 1941, the first of the  
fourth series of tests was carried out. The  
results of this test are given in Table 1.  
The results of the other three tests of the  
fourth series are given in Tables 2, 3 and 4.  
The results of the first three tests of the  
fifth series are given in Tables 5, 6 and 7.  
The results of the other two tests of the  
fifth series are given in Tables 8 and 9.  
The results of the first two tests of the  
sixth series are given in Tables 10 and 11.  
The results of the other three tests of the  
sixth series are given in Tables 12, 13 and 14.

The results of the first two tests of the  
seventh series are given in Tables 15 and 16.  
The results of the other three tests of the  
seventh series are given in Tables 17, 18 and 19.  
The results of the first two tests of the  
eighth series are given in Tables 20 and 21.  
The results of the other three tests of the  
eighth series are given in Tables 22, 23 and 24.

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